

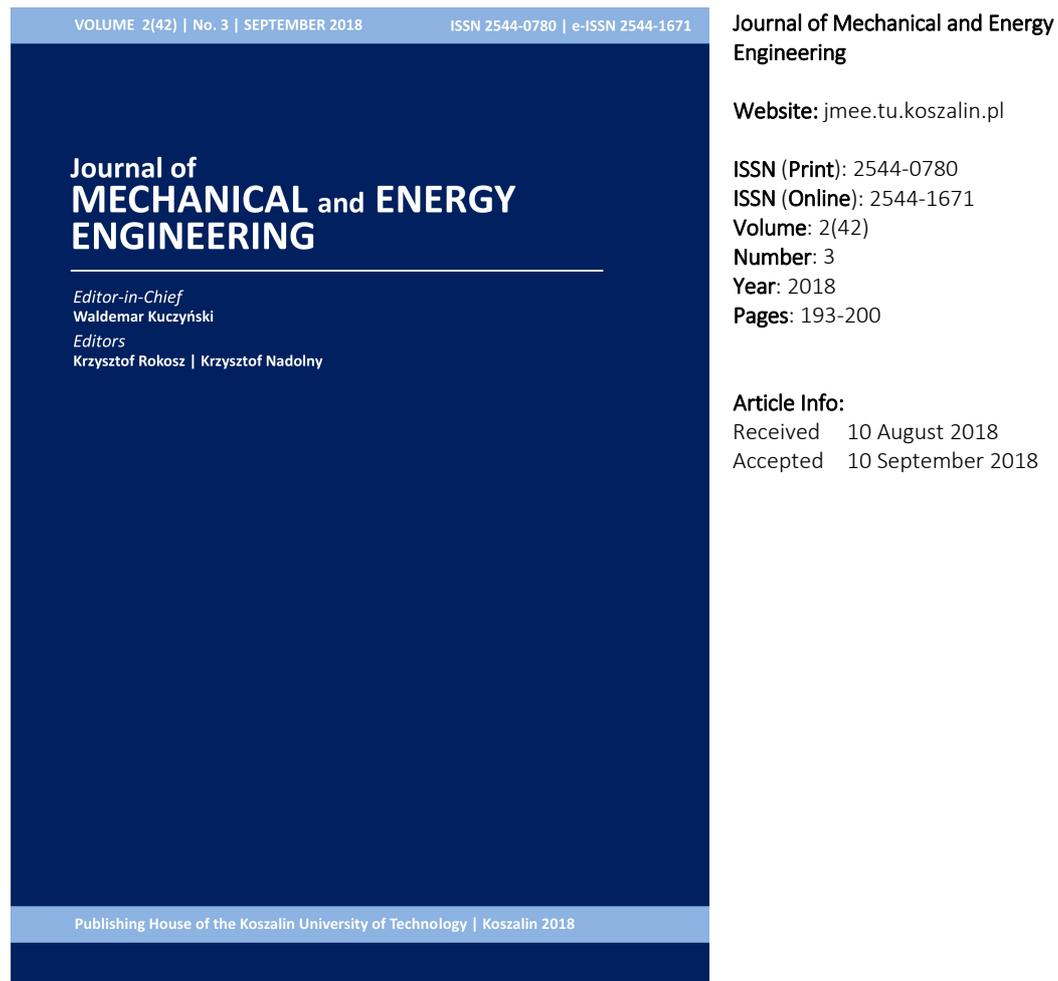
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# PARAMETRIC STUDY OF ELECTROCHEMICAL DISCHARGE DRILLING ON CERAMIC MATERIAL USING TAGUCHI METHOD

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**Abstract:** The Electrochemical Discharge machining (ECDM) is a hybrid machining technology which is combined with electro discharge machining and electro chemical machining process. In this research, electrochemical discharge drilling operation is carried out on conventional ceramic tile by using a designed and manufactured ECDM setup. The experiments were performed as per design of experimental technique of Taguchi L<sub>27</sub> orthogonal array using MINITAB 17 software. The important process parameters that have been selected are voltage, rotation and electrolyte concentration with output response as machining depth and diametric cut. From the observations, it is found that the voltage is the most significant parameter for the machining depth and diametric cut followed by electrolyte concentration and rotation.

**Keywords:** diametric cut, electrochemical discharge drilling, machining depth, ceramic, Taguchi

## 1. INTRODUCTION

The materials of composites and ceramics can be machined with a combination of advanced conventional and non-conventional manufacturing processes. These machining processes create changes in size, shape, and surface finish to get a high-quality product [1]. The electrochemical discharge machining (ECDM) process firstly introduced in the year 1968 by Kurafuji through attempting micro drilling on glass material [2]. The ECDM technology is a combination of two machining processes which include the electro discharge machining process (EDM) and the electrochemical machining (ECM) process. The erosion of material is taking place because of two phenomena, i.e. electrochemical dissolution of the material and thermal erosion of electrical discharges that take place between the anode and cathode tool electrodes [3]. The ECDM technology can be excellently utilized for the machining of non-conductive materials like ceramics, glass and advanced composites. In this process, the spark discharge exploits across the gas bubble layers

produced on the workpiece surface, and therefore, erosion of material takes place [4]. The ECDM process is also called as spark assisted chemical engraving process and electrochemical spark machining process. The process can be effectively used in the field of MEMS interfacing, microfactories, and micro fluidic devices [5]. In this machining technology, researchers have commonly utilized NaOH as an electrolyte chemical solution, Tungsten carbide as a cathode tool electrode material and Graphite as an anode tool electrode material [6]. The voltage is an utmost key factor for material removal rate then the electrolyte concentration is secondary significant parameter and last is inter electrode gap [7]. The gas film is vital for ECDM process, but the stability and dynamics of this film conditions are also important during the machining process [8]. The deeper hole drilling is achieved and controlled by the hydrodynamic regime; however, the speed of drilling is limited by the flow of electrolyte inside the micro-hole [9]. The machined hole circularity increases due to rotation of tool electrode, but it is not dominant factor like voltage [10]. The voltage is most significant factor for radial overcut during ECDM micro drilling

operation [11]. The material removal rate and machined depth were enhanced due to abrasive tool electrodes in the electrochemical spark abrasive drilling process [12]. Likewise, the rotary abrasive tool electrode has improved cutting and machining ability due to the presence of abrasive grains in the drilling actions on Al<sub>2</sub>O<sub>3</sub> material [13]. The flat sidewall–flat front tool in the ECDCM micro drilling process enhances the machining accuracy. As well as, the rotational rate of the tool has improved the process performance [14]. The change in tool rotational speed has minute influence on the ECDCM process parameters. Also, gas film formation time drops and tends to be a minimum by rise in voltage [15]. The voltage, inter electrode gap and electrolyte concentration were the dominant factors in consequence on output responses of radial overcut and material removal rate [16]. The KOH electrolyte produces higher bubbles than H<sub>2</sub>SO<sub>4</sub> electrolyte solution therefore it gives higher material removal rate. [17]. The finite element method explicit dynamics ANSYS was used for analysis of different material in electrochemical discharge machine structure [18]. Similarly, Goud et al. analysed material removal rate in electrochemical discharge machining using a three-dimensional finite element method [19]

Previously, Pawar et al. investigated material removal rate and tool wear rate during machining of ceramic material and he also investigated material removal rate of soda-lime glass material [20, 21]. In this paper, the investigated diametric cut and machining depth during drilling on ceramic material by using the ECDCM process with the same input data of Pawar et al. So, this paper is a continuation of previously carried out experimental works.

### 1.1. Basic Mechanism of ECDCM

The ECDCM process shown in Fig. 1 a high voltage DC power supply was used for the machining process, and aqueous solution of hydroxides was utilized as electrolyte in ECDCM cell. In this process, voltage was increased in the range of 0-12 V.

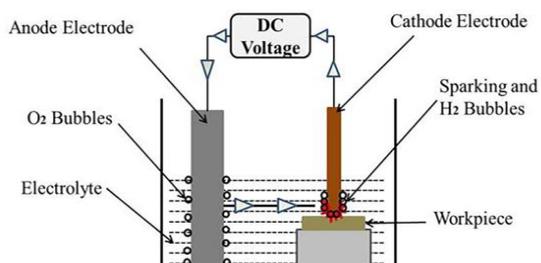


Fig. 1. Basic mechanism of ECDCM process

The electrolysis with gas bubbles is formed at the electrode around surfaces. At the stage of higher voltage, a maximum critical current value take place. This is because of high intensity of hydrogen bubbles produced at the cathode being coalesced to generate a

film on tool. Then, with further rise in voltage, the current fell down to a lower value due to film creation of gas bubbles. Finally, increase in voltage causes breaking of gas film to produce spark because of high intensity flow of electrons from cathode to electrolyte [22].

## 2. EXPERIMENTAL SETUP AND EXPERIMENTAL PROCEDURE

The ECDCM schematic diagram and machine setup was designed and developed which is presented in Figure 2 and Figure 3.

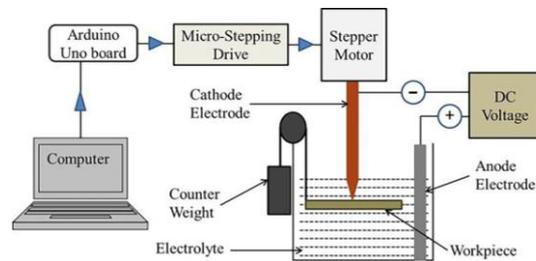


Fig. 2. Schematic diagram of ECDCM setup

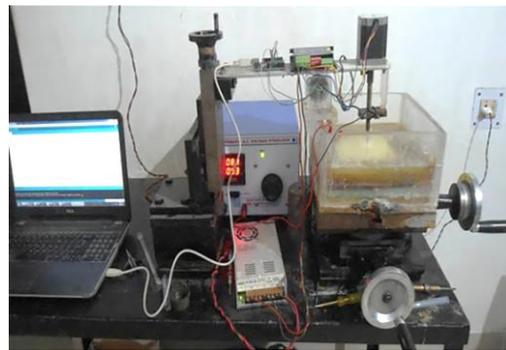


Fig. 3. Fabricated experimental ECDCM setup

This machine is fabricated by using 2D drawings and 3D model [23]. The experimental setup of ECDCM consists of X-Y stage for manual movement on the base platform which was used to move the workpiece. The workpiece was fixed on a holding fixture. The gravity loaded mechanism was used for the movement of the workpiece from lower to upper Z axis movement. A rectangular tank made up of acrylic material was used as ECDCM cell which contains NaOH electrolyte solution, cathode and anode tool electrodes. The single axis slide system was used as Z axis movement which was fixed to the table. The NEMA 23 stepper motor was attached to the flat beam which was attached to the top position of a single axis slide system. The cathode tool electrode attached to spindle of stepper motor, and this motor was connected to micro-stepping drive. This micro-stepping drive was connected to Arduino Uno board, and Arduino Uno board was connected to computer. The rotating movement of cathode tool electrode was controlled by using Arduino software programming

through computer and Z axis movement from cathode tool to workpiece was operated manually.

The gravity feeding mechanism was applied to the workpiece which moved upwards to cathode electrode tool tip point. The regulated DC voltage source was used to supply DC voltage between cathode tool electrode and an auxiliary tool electrode. The stainless steel 416 rod was used as an anode electrode which was put into an electrolyte container. Figure 4 shows spark generation during micro drilling of conventional ceramic in ECDM process.



Fig. 4. Sparking during ECDM drilling on ceramic

**2.1. Experimental Conditions**

The experiments were carried out based on Taguchi L<sub>27</sub> orthogonal array with process parameters as voltage, rotation and electrolyte concentration which are varied in three levels shown in Table 1. The

machining depth and diametric cut are taken as output responses. The machining depth and diametric cut was measured by using digital Vernier caliper. The experiments were performed with 150×125×8 mm<sup>3</sup> conventional ceramic tile as workpiece material and using conical shaped 3 mm diameter brass cathode tool electrode. The starting point tool diameter was 1 mm and its diameter increased up to 3 mm due to conical shape given to the tool electrode. The conical shape length of 5 mm. The experimental work was conducted on a fabricated electrochemical discharge machine. The NaOH was used as an electrolyte medium. The machining time was set to be 25 minutes for each experiment. The inter electrode gap between the cathode and anode tool was kept constant for all experiments. The tabulated format of the results is shown in Table 2, which depicts the process parameter and output responses. The S/N ratio indicates the higher value which signifying better machining performance such as for machining depth, ‘higher-the-better’ and diametric cut, ‘nominal is best’. Figure 5 and figure 6 show the experimental results and their microscopic images. The S/N ratio is calculated from experimental data which provide measures of robustness to identify the control factors that reduce the variability of process. The S/N ratio formula for machining depth higher the better is shown in Eq. 1 [22]:

$$S / N = -10 \log \left( \frac{1}{n} \sum_{i=1}^n \frac{1}{y_i^2} \right). \quad (1)$$

Tab. 1. Input Process parameters and their levels

Factor	Parameters	Unit	Levels		
			1	2	3
A	Voltage	V	70	80	90
B	Rotation	r/min	10	15	40
C	Electrolyte Concentration	%	5	10	15



Fig. 5. Experimental results of ceramic material using ECDM

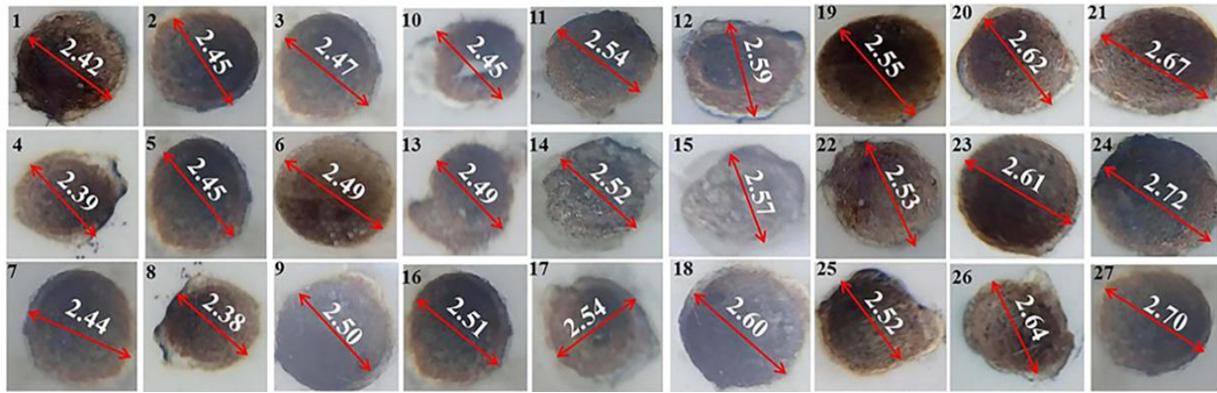


Fig. 6. Microscopic images of experimental results of ceramic material using ECDM

Tab. 2. Experimental results

Run	Voltage	Rotation	Electrolyte Concentration	Machining Depth (mm)	Diametric cut (mm)
1	70	10	5	0.95	2.42
2	70	10	10	1.01	2.45
3	70	10	15	1.10	2.47
4	70	25	5	0.99	2.39
5	70	25	10	1.05	2.45
6	70	25	15	1.15	2.49
7	70	40	5	1.01	2.44
8	70	40	10	1.10	2.38
9	70	40	15	1.20	2.50
10	80	10	5	1.15	2.45
11	80	10	10	1.28	2.54
12	80	10	15	1.37	2.59
13	80	25	5	1.14	2.49
14	80	25	10	1.30	2.52
15	80	25	15	1.37	2.57
16	80	40	5	1.17	2.51
17	80	40	10	1.31	2.54
18	80	40	15	1.41	2.60
19	90	10	5	1.27	2.55
20	90	10	10	1.37	2.62
21	90	10	15	1.45	2.67
22	90	25	5	1.30	2.53
23	90	25	10	1.45	2.61
24	90	25	15	1.52	2.72
25	90	40	5	1.32	2.52
26	90	40	10	1.47	2.64
27	90	40	15	1.58	2.70

### 3. RESULTS AND DISCUSSION

In the Taguchi technique, the least difference and the optimal parameters are attained by means of the  $S/N$  ratio. The delta value represents the difference between the highest and lowest average assessment of  $S/N$  ratio for each factor. The analysis was done using MINITAB 17 software.

#### 3.1. Effect on Machining depth

The mean  $S/N$  ratios plot denotes the influence of each parameter on machining depth. Fig. 7 shows the

influence of the three different parameters viz. voltage, rotation and electrolyte concentration on the machining depth output response. The following figures demonstrate the linear increase in voltage resulting increase in machining depth; therefore it is the most significant parameter. From the experimental results, it is observed that the maximum machining depth increases with increasing applied voltage and electrolyte concentration, it may be due to generation of more electrical discharge from bottom of brass tool towards workpiece [24].

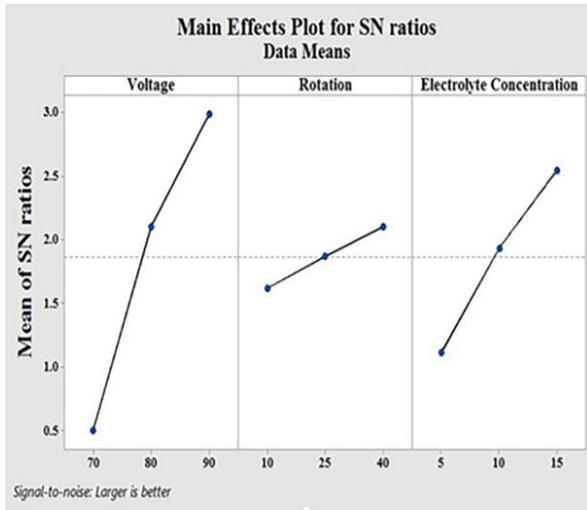


Fig. 7. Mean S/N ratios plot for machining depth

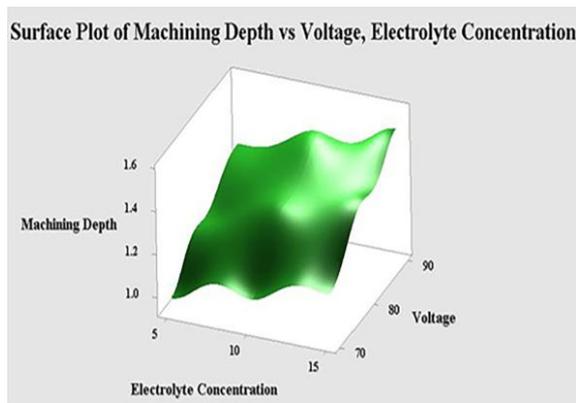


Fig. 8. Surface plot of machining depth vs. voltage, electrolyte concentration

Fig. 8 and Fig. 9 shows surface plot for machining depth. It represents the effect of voltage, rotation and electrolyte concentration on the machining depth.

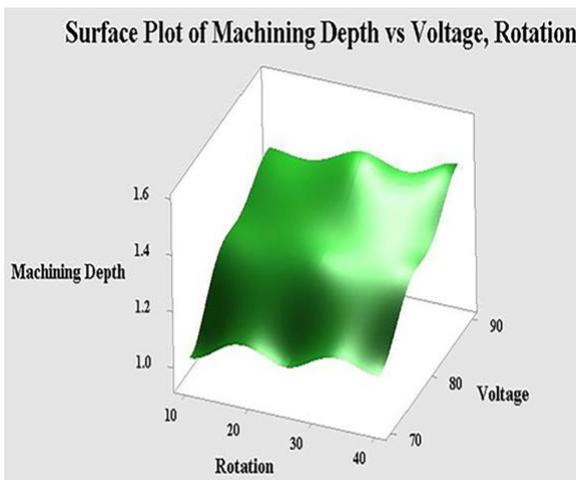


Fig. 9. Surface plot of machining depth vs. voltage, rotation

Table 3 shows ANOVA Table for machining depth. If *p* value is smaller than 0.05 then the parameter is significant, here voltage, electrolyte concentration and rotation of tool electrode are the most significant

parameters. Table 4 shows the average of each response characteristic for each level of each factor. This table specifies the ranks based on delta measurements and Minitab 17 allocates ranks based on delta values; rank 1 to the highest delta value, rank 2 to the second highest and, so on. The ranks designate the significance of each factor in the response. The ranks and delta values confirmed that the voltage has the greatest effect on machining depth followed by electrolyte concentration and rotation.

Tab. 3. ANOVA table for machining depth

Source	df	Adj SS	Ad MS	F Value	P Value
Voltage	2	0.5676	0.2838	455.84	0.00
Rotation	2	0.0213	0.0106	17.16	0.07
Electrolyte Concentration	2	0.1911	0.0955	153.49	0.00
Error	20	0.0124	0.0006		
Total	26	0.792			
S		R-Sq.	R-sq.(adj.)	R-sq.(pred.)	
		0.0249518	98.43 %	97.96%	97.14%

Tab. 4. Response table for signal to noise ratios of machined depth

Level	Voltage	Rotation	Electrolyte Concentration
1	0.5019	1.6221	1.1151
2	2.1042	1.8717	1.9350
3	2.9902	2.1025	2.5462
Delta	2.4883	0.4804	1.4311
Rank	1	3	2

Eq. (2) shows mathematical model for the machining depth developed by using MINITAB 17 software:

$$Machining.Depth = -0.4204 + 0.017611 * Voltage + 0.00229 * Rotation + 0.02056 * Electrolyte \cdot Concentration \quad (2)$$

### 3.2. Effect on Diametric cut

The means of mean plot denotes the influence of each parameter on diametric cut. Figure 10 presents the influence of three different parameters viz. voltage, rotation and electrolyte concentration on the diametric cut output response. The following figures indicate the linear increase in voltage resulting increase in diametric cut therefore it is the most significant parameter. The voltage and electrolyte concentration are the most dominant factors for the diametric cut [25]. Eq. 3 shows a mathematical model for the

diametric cut developed by using MINITAB 14 software:

$$Diametric \cdot Cut = 1.7154 + 0.008722 * Voltage + 0.00025 * Rotation + 0.013 * Electrolyte \cdot Concentration \quad (3)$$

Fig. 11 and Fig. 12 shows the surface plot for diametric cut. It represents the effect of voltage, rotation and electrolyte concentration on the diametric cut.

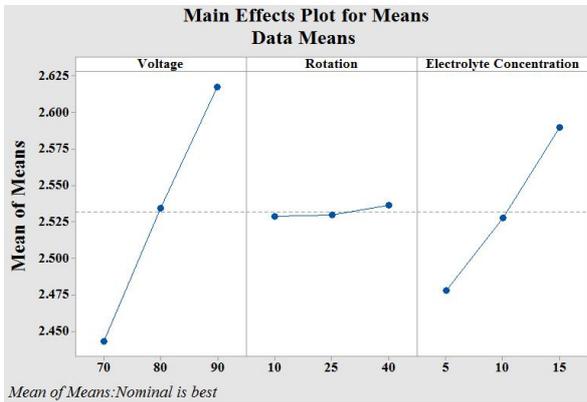


Fig. 10. Mean S/N ratios plot for diametric cut

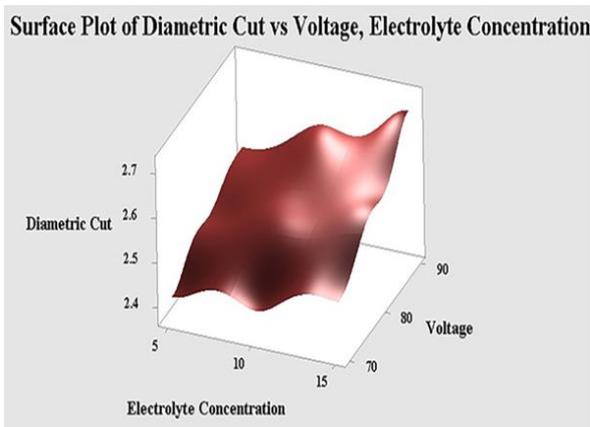


Fig. 11. Surface plot of diametric cut vs voltage, electrolyte concentration

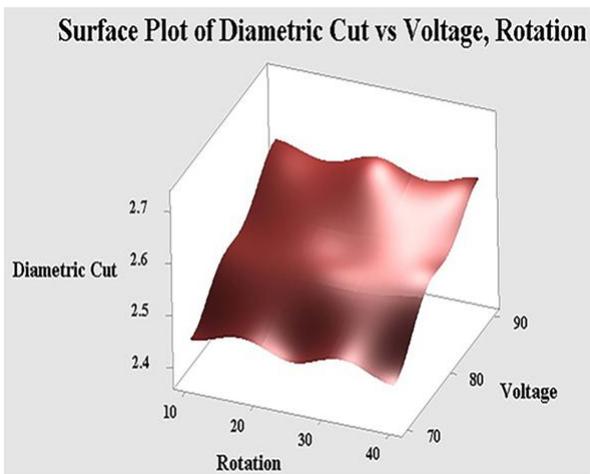


Fig. 12. Surface plot of diametric cut vs voltage, rotation

Table 5 shows ANOVA Table for diametric cut. If  $p$  value is smaller than 0.05, then the parameter is significant, here voltage and electrolyte concentration are the most significant parameters. The response Table 6 depicts the response for means of diametric cut for each level of each factor. The ranks and delta values confirmed that the voltage has greatest effect on diametric cut and is followed by electrolyte concentration and rotation.

Tab. 5. ANOVA table for diametric cut

Source	df	Adj SS	Adj MS	F-Value	P-Value
Voltage	2	0.1370	0.06851	78.92	0.00
Rotation	2	0.0003	0.00015	0.18	0.834
Electrolyte Concentration	2	0.0568	0.02844	32.77	0.00
Error	20	0.0173	0.00086		
Total	26				

S	R-Sq.	R-sq.(adj.)	R-sq.(pred.)
0.029	91.79%	89.33%	85.05%

Tab. 6. Response table for means of diametric cut

Level	Voltage	Rotation	Electrolyte Concentration
1	2.443	2.529	2.478
2	2.534	2.530	2.528
3	2.618	2.537	2.590
Delta	0.174	0.008	0.112
Rank	1	3	2

#### 4. CONCLUSIONS

The designed and manufactured electrochemical discharge machine setup was used for the present experimental investigation. In this work, two output responses i.e. machining depth and diametric cut were investigated by varying the three input process parameters on a conventional ceramic tile with Brass as a cathode electrode in an electrochemical discharge machine. The input parameters considered as voltage, rotation and electrolyte concentration. The experiments were conducted according to Taguchi L<sub>27</sub> orthogonal array design. From the present study, it can be concluded that the voltage and electrolyte concentration are the most dominant factors for machining depth and diametric cut. However, rotation was the least significant factor for machining depth and diametric cut. The optimum parameters of the combination setting are Voltage 90V, Rotation 40r/min, and Electrolyte concentration 15% for the maximum machining depth and nominal diametric cut.

## Nomenclature

<i>ECDM</i>	– electrochemical discharge machining
<i>S/N ratio</i>	– signal to noise ratio
<i>ANOVA</i>	– analysis of variance
<i>r/min</i>	– rotation per minute
<i>df</i>	– degree of freedom
<i>n</i>	– number of measurements
<i>y<sub>i</sub></i>	– measured values
<i>Adj SS</i>	– adjusted sum of squares
<i>Adj MS</i>	– adjusted mean squares
<i>F-Value</i>	– statistical value
<i>P-Value</i>	– probability value
<i>DC voltage</i>	– direct current voltage
<i>mm</i>	– millimeter
<i>S</i>	– response variable
<i>R-Sq.</i>	– percentage variation in response
<i>R-sq.(adj.)</i>	– adjusted percentage variation in response
<i>R-sq.(pred.)</i>	– predicted percentage variation in response

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## Biographical notes



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